

# Electrochemical properties of dye-sensitized solar cells fabricated with PVDF-type polymeric solid electrolytes

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## Abstract

We have already proposed a poly(vinylidene fluoride-co-hexafluoropropylene) (PVDF-HFP)-based polymeric solid electrolyte (PSE) film for dye-sensitized solar cells (DSSCs). The employment of the PSE film, however, almost always accompanies with decrease in short-circuit current density ( $J_{sc}$ ). We then studied electrochemical properties on the PSE-based and liquid electrolyte-based DSSCs to clarify the reason why the conversion efficiency is lower in the former than in the latter. The diffusion coefficient of  $I_3^-$  and the cell gap of DSSCs were found out to play a key role to increase  $J_{sc}$ . In particular, the stronger cell-gap dependence was observed in the PSE-based DSSC than in the liquid electrolyte-based DSSC. This indicates that the design of DSSC structure is quite important to achieve the higher conversion efficiency in the PSE-based DSSC. We confirmed that the  $J_{sc}$  of a PSE-based DSSC with a 20  $\mu\text{m}$  cell gap is turned out to be about 97% of the  $J_{sc}$  of a liquid electrolyte-based DSSC.

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**Keywords:** PVDF; DSSC; Electrolyte; Polymeric solid electrolyte

## 1. Introduction

Dye-sensitized solar cells (DSSCs) were first studied extensively by Tsubomura et al. in 1976 [1]. The conversion efficiency of the solar cells was then about 1%. O'Regan and Grätzel made a major breakthrough in the conversion efficiency in 1991 [2] and opened up the possibilities of practical applications as solar cells. A DSSC comprises an electrode consisting of a nanocrystalline  $\text{TiO}_2$  layer with ruthenium sensitizer adsorbed on the  $\text{TiO}_2$  surface, a counter electrode consisting of a F-doped  $\text{SnO}_2$  substrate with a Pt thin layer coated on top of it, and an electrolyte solution with a  $I^-/I_3^-$  redox couple.

DSSCs are attractive for next-generation solar cells not only because of their potentially high conversion efficiency but also because of the lower production cost of DSSCs than that of conventional silicon solar cells [3]. However, many things, such as increasing the conversion efficiency even more and achieving better durability, remain to be done before DSSCs can be put on the market [4–8]. The electrolyte loss caused by the leakage and/or volatility of the electrolyte solution has been pointed out to be one of the major problems, which stays the durability of the DSSC low. Various

approaches to the problem have been tried so far. These approaches include employing a gel-type electrolyte to minimize the loss [9–13], or replacing the liquid electrolyte with either p-type solid inorganic semiconductors or conducting organic materials to avoid the loss completely [14–22]. The gel-type electrolyte appears to give rise to successful results in terms of a conversion efficiency among these approaches. Wang et al. recently employed a polymeric gel electrolyte containing 1-methyl-3-propylimidazolium iodide and poly(vinylidene fluoride-co-hexafluoropropylene) (PVDF-HFP) to fabricate a DSSC, and the conversion efficiency of that DSSC with a 0.152  $\text{cm}^2$  active area at AM 1.5 illumination stayed at 5.3% [23]. We proposed a PVDF-HFP-based polymeric solid electrolyte (PSE) film for DSSCs [24,25]. The film allows us to obtain a short-circuit current density ( $J_{sc}$ ) higher than 70% of that of a DSSC with a liquid electrolyte. Although these measures are effective in reducing or avoiding electrolyte loss, they almost always cause the conversion efficiency to decrease.

The purpose of this paper is two-fold: (1) we elucidate the reason why the conversion efficiency is lower in PSE-based DSSCs than in liquid electrolyte-based DSSCs, and (2) obtain a guiding principle for the design of the PSE-based DSSC with a high enough conversion efficiency and equal to that of the liquid electrolyte-based DSSC.

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## 2. Experimental

All reagents were commercially available and used as-purchased. TiO<sub>2</sub> paste (Ti-nanoxide-T, Solaronix) was coated on a F-doped SnO<sub>2</sub> (FTO) substrate (TEC15, about 15 Ω/sq, Pilkington) using a Baker-applicator. The thickness of an as-coated TiO<sub>2</sub> film is about 250 μm and was then pre-cured at about 90 °C followed by heat treatment at 450 °C for 1 h. The TiO<sub>2</sub> films formed on the FTO were 10 μm thick and 5 mm × 5 mm in size. The TiO<sub>2</sub> substrate was immersed in ruthenium sensitizer (referred to hereafter as “dye”) solution (0.5 mmol/l ruthenium-535-bis-TBA, Solaronix, in EtOH) for 20 h to let the nanosized-TiO<sub>2</sub> layer adsorb the dye, and the excess amount of dye was then rinsed off with EtOH. A 30 nm thick Pt thin film was deposited on the FTO substrate with the ion plating method, and was used as a counter electrode.

The electrolyte solution used in the liquid electrolyte-based DSSC is composed of 0.5 mol/l 1-propyl-2,3-dimethylimidazolium iodide (DMPII), 0.1 mol/l LiI, 0.05 mol/l I<sub>2</sub>, 0.5 mol/l 4-*tert*-butylpyridine (TBP), and one of the following solvents to change the viscosity of the electrolyte solution and thus to change the diffusion coefficient of I<sub>3</sub><sup>−</sup>: methoxyacetonitrile (MAN), 3-methoxypropionitrile (MPN),  $\gamma$ -butyrolactone (GBL), and propylene carbonate (PC). The viscosity of the solvent was measured at 25 °C with a viscosity meter (Viscomate VM-1G, Yamaichi electronics Co. Ltd.). The PSE film consists in the PVDF-HFP-based matrix polymer and an electrolyte solution (0.5 mol/l 1-propyl-2,3-dimethylimidazolium iodide, 0.1 mol/l LiI, 0.05 mol/l I<sub>2</sub>, and 0.5 mol/l 4-*tert*-butylpyridine in  $\gamma$ -butyrolactone). The electrolyte solution and the matrix polymer were mixed with various contents depending on the purpose, and acetone was added to the mixture. The mixture was stirred at 70 °C until the polymer was dissolved completely. The mixture was then coated on a substrate with a doctor blade and left for 20 min at room temperature to dry. <sup>1</sup>H NMR analysis (JEOL EX-400) was carried out on a PSE film dissolved in dimethyl-d<sub>6</sub> sulfoxide, which confirmed no acetone residue in the film. The melting point was determined with a differential scanning calorimeter (Perkin Elmer DSC7). The polymer content of the PSE film was determined from the weight ratio of an as-formed PSE film to a dried, electrolyte-solution-free film. The diffusion coefficients ( $D_s$ ) of I<sub>3</sub><sup>−</sup> in the PSE films were evaluated using the Cottrell equation,  $i(t) = nFAD^{1/2}C_0/\pi^{1/2}t^{1/2}$ , where  $n = 2$ ,  $F$  is the Faraday constant,  $C_0$  the initial concentration of I<sub>3</sub><sup>−</sup>, with the current decay curve obtained after applying a 0.6 V potential to a FTO/Pt/electrolyte/Pt/FTO cell [26].

The PSE-based DSSC was assembled by sandwiching a PSE film between the TiO<sub>2</sub>-dye electrode and a Pt counter electrode and then sealing the perimeter of the cell while pressurizing it. The cell gap of the PSE-based DSSC was selected by changing the thickness of the PSE film to be prepared. The liquid electrolyte-based DSSC was assembled as follows: the two electrodes were held together with two

pieces of a PET (polyethylene terephthalate) strips placed between the edges of the two electrodes; an electrolyte solution was introduced between the electrodes by capillary forces; the cell was then sealed along its perimeter. The cell gaps thus selected by tuning the thickness of the PET strips were measured with a micrometer (MDQ-30 Mitsutoyo Corporation). The cell gaps used are the length between the surfaces of the two FTO substrates.

The  $I$ - $V$  characteristics were measured with a potentiostat (Schlumberger 1287 Solartron) under illumination (AM 1.5, 100 mW/cm<sup>2</sup>, surface temperature of the DSSC at 27 °C) using a solar simulator (YSS-150, Yamashita-Denso Co. Ltd.) equipped with a cooling stage.  $I$ - $V$  curves were obtained by scanning an applied potential to the DSSC between 1.5 and −0.5 V at a scan rate of 10 mV/s. Electrical impedance spectra were obtained in the frequency region from 10<sup>−2</sup> to 10<sup>6</sup> Hz under illumination by applying sinusoidal perturbations of ±5 mV superimposed on the open-circuit voltage ( $V_{oc}$ ). The electrical impedance spectra were analyzed using Z-View software (Solartron).

## 3. Results and discussion

### 3.1. Influence of the diffusion coefficient of I<sub>3</sub><sup>−</sup> on the $J_{sc}$ of DSSCs

The  $J_{sc}$  and  $V_{oc}$  values and diffusion coefficients of I<sub>3</sub><sup>−</sup> of the liquid electrolyte-based and PSE-based DSSCs, and viscosities of the liquid electrolyte are tabulated in Table 1. The diffusion coefficients of the liquid electrolytes depend on their respective solvent (MAN, MPN, PC and GBL) viscosities, while those of the PSE film depend on the polymer contents (GBL/matrix polymer = 20.7, 27.5 and 37.0 mass%). In Fig. 1, the  $J_{sc}$  values given in Table 1 are plotted with the diffusion coefficient of I<sub>3</sub><sup>−</sup>. The  $J_{sc}$ 's sharply increase with the diffusion coefficient and level off for larger values of the diffusion coefficient. The decrease in the diffusion coefficient reduces the supply of I<sub>3</sub><sup>−</sup> to the Pt counter electrode, causing the depletion of I<sub>3</sub><sup>−</sup> at the electrode and therefore

Table 1

The  $J_{sc}$  and  $V_{oc}$  values and diffusion coefficients of I<sub>3</sub><sup>−</sup> of the liquid electrolyte-based and PSE-based DSSCs, and viscosities of the liquid electrolyte

| Liquid electrolyte                               | $D$ ( $\times 10^6$ cm <sup>2</sup> /s) | $J_{sc}$ (mA/cm <sup>2</sup> ) | $V_{oc}$ (V) | Viscosity (mPa s) |
|--|---|--------------------------------|--------------|-------------------|
| MAN  | 7.56                                    | 13.79                          | 0.74         | 1.70              |
| MPN  | 5.39                                    | 12.70                          | 0.73         | 2.47              |
| GBL  | 3.94                                    | 11.60                          | 0.75         | 3.29              |
| PC   | 2.72                                    | 10.02                          | 0.70         | 4.64              |
| PSE (GBL/matrix polymer) polymer content (mass%) |   |                                |              |                   |
| 20.7   | 2.26                                    | 10.75                          | 0.75         | –                 |
| 27.5   | 1.90                                    | 10.10                          | 0.70         | –                 |
| 37.0   | 1.06                                    | 6.28                           | 0.75         | –                 |

MAN: methoxyacetonitrile, MPN: 3-methoxypropionitrile, GBL:  $\gamma$ -butyrolactone, and PC: propylene carbonate.

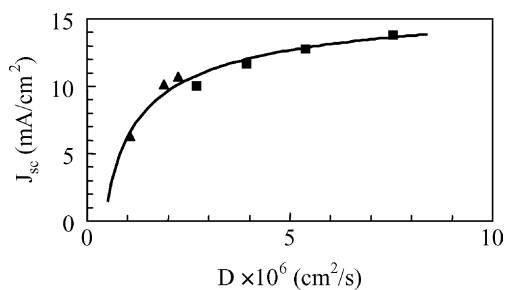


Fig. 1. Short-circuit current density ( $J_{sc}$ ) of liquid electrolyte-based and PSE-based DSSCs with different diffusion coefficients of  $I_3^-$ : (■) liquid electrolyte-based DSSC; (▲) PSE-based DSSC.

decreasing the  $J_{sc}$ . The ionic conductivity of the electrolyte,  $\sigma = ne\mu$ , is related to the diffusion coefficient of the supporting electrolyte through Einstein's relation,  $D = \mu kT$ : in the two equations,  $n$  is the carrier density,  $\mu$  the mobility,  $k$  Boltzmann constant and  $T$  the temperature [27]. The decrease in the  $J_{sc}$  might originate from the decrease in the ionic conductivity. On the other hand, the  $J_{sc}$  tends to level off with increasing diffusion coefficient is caused mainly by the limited numbers of electrons available from the dye which is in turn limited by the absorption spectrum of the dye, i.e., photon limiting case.

As in Fig. 2, the diffusion coefficient dependence of the  $V_{oc}$  that we observed is quite weak and its variation is within 4%. The reverse-electron transfer from  $TiO_2$  to  $I_3^-$  is reported to reduce  $V_{oc}$  because the electron density in the conduction band of  $TiO_2$  decreases [28]. In an open-circuit condition, the concentration of  $I_3^-$  is expected to be constant over the entire distance between the  $TiO_2$  and Pt counter electrodes irrespective of the diffusion coefficient of  $I_3^-$ . Hence, the  $V_{oc}$  is independent of the diffusion coefficient of  $I_3^-$ .

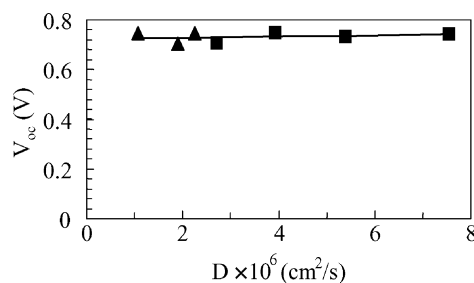


Fig. 2. Open-circuit voltage ( $V_{oc}$ ) of liquid electrolyte-based and PSE-based DSSCs with different diffusion coefficients of  $I_3^-$ : (■) liquid electrolyte-based DSSC; (▲) PSE-based DSSC.

There is a possibility that the reverse-electron transfer is responsible for decreasing the  $J_{sc}$ . However, a close study still needs to be carried out on the electro- and photochemistry at the  $TiO_2$ /dye/electrolyte interface, combined with relevant model equations for the reactions inside the DSSC, to interpret the role of the reverse-electron transfer reaction in determining the  $J_{sc}$ .

Fig. 3 shows the electrical impedance spectra of the PSE-based DSSCs with five different polymer contents. All of the electrical impedance spectra exhibit three semicircles (A, B, and C), which are assigned, respectively, to the electrochemical reaction at the Pt counter electrode, the reaction at the  $TiO_2$ /dye electrode, and the diffusion process of  $I_3^-$  at the Pt/electrolyte interface [24,29]. We employed the equivalent circuit given in Fig. 4 for the curve fitting of the impedance spectra of DSSCs. The parameters obtained by fitting the impedance spectra with this equivalent circuit are summarized in Table 2. The symbol  $R_i$  ( $i = 1, 2$ ) indicates the charge transfer resistance of the electrochemical reaction;  $R_s$  is the series resistance composed of the resistance of the electrolyte,  $TiO_2$ , the sheet resistance of the FTO film, and so

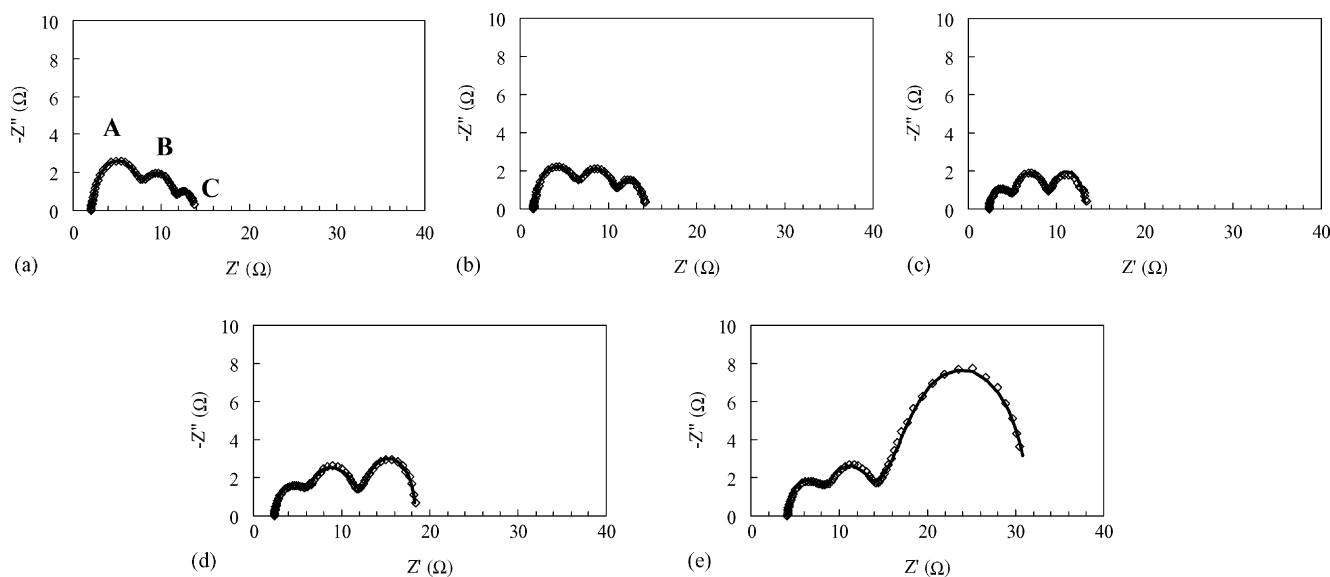


Fig. 3. Electrical impedance spectra of DSSCs with five different polymer contents: (a) 0 mass%; (b) 22.1 mass%; (c) 26.3 mass%; (d) 32.8 mass%; (e) 48.1 mass%.

Table 2

Numerical values for each element in the equivalent circuit obtained on DSSCs with five different polymer contents

| Polymer content (mass%) | $R_s$ ( $\Omega$ ) | $R_1$ ( $\Omega$ ) | $R_D$ ( $\Omega$ ) | $\tau$ (s) | $T_1$ (mF) | $P_1$ | $R_2$ ( $\Omega$ ) | $T_2$ (mF) | $P_2$ |
|-------------------------|--------------------|--------------------|--------------------|------------|------------|-------|--------------------|------------|-------|
| 0                       | 2.05               | 5.69               | 2.42               | 0.86       | 0.061      | 0.91  | 3.66               | 2.57       | 0.92  |
| 22.1                    | 1.50               | 4.86               | 3.49               | 1.08       | 0.074      | 0.90  | 4.12               | 2.97       | 0.89  |
| 26.3                    | 1.92               | 3.54               | 4.43               | 1.82       | 0.051      | 0.94  | 3.80               | 3.12       | 0.90  |
| 32.8                    | 2.37               | 3.53               | 7.10               | 3.62       | 0.147      | 0.87  | 5.36               | 3.15       | 0.87  |
| 48.1                    | 4.15               | 4.04               | 18.31              | 8.58       | 0.085      | 0.89  | 5.04               | 2.54       | 0.88  |

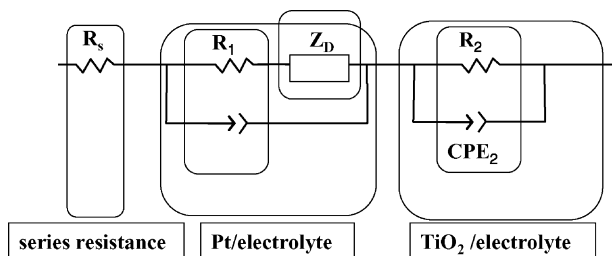
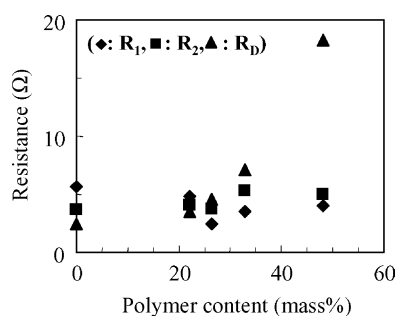
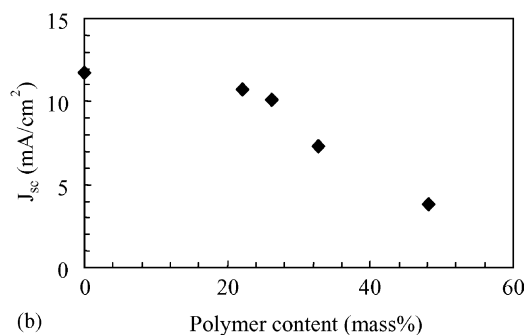
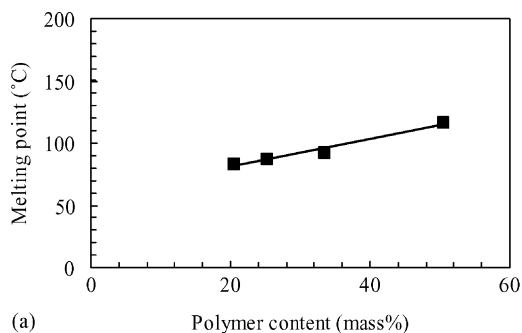
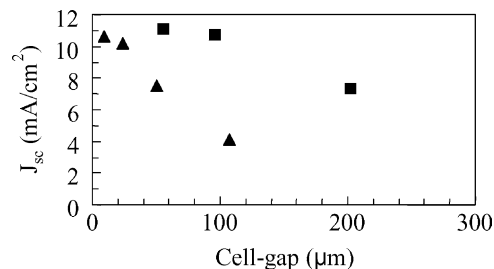


Fig. 4. Equivalent circuit model of the impedance spectra of DSSCs.

Fig. 5. Polymer content dependence of the resistance of the Pt/PSE interface ( $R_1$ ), the resistance of the  $\text{TiO}_2$ /PSE interface ( $R_2$ ), and the diffusion resistance ( $R_D$ ).

on;  $Z_D$  the finite-length Warburg diffusion impedance; and  $\text{CPE}_i$  ( $i = 1, 2$ ) the constant phase element. The impedance of the Warburg diffusion in a finite-length region and  $\text{CPE}_i$  are defined, respectively, by the following equations:

$$Z_D = R_D \left\{ \frac{[\tanh(j\omega\tau)^{1/2}]}{(j\omega\tau)^{1/2}} \right\} \quad (1)$$

Fig. 7. Melting points of PSE films and the  $J_{sc}$  of DSSCs with five different polymer contents.Fig. 6. Dependence of the  $J_{sc}$  on the cell gap of liquid electrolyte-based and PSE-based DSSCs: (■) liquid electrolyte-based DSSC; (▲) PSE-based DSSC.

where  $\tau = L^2/D_e$ ,  $D_e$  is the effective diffusion coefficient of the diffusing species, and  $L$  the effective length:

$$\text{CPE}_i = \frac{1}{T_i(j\omega)^{P_i}} \quad (2)$$

where  $T_i$  and  $P_i$  are parameters obtained by curve fitting. Detailed discussions of these parameters are given elsewhere [24]. The resistances of the Pt/PSE interface ( $R_1$ ) are plotted in Fig. 5.  $R_1$ , unlike the diffusion coefficient, depends hardly on the polymer content.  $R_1$  is the charge transfer resistance at the interface between the PSE film and the Pt counter electrode. Therefore, the decrease in the  $J_{sc}$  of the two different kinds of DSSC, given in Fig. 2, results mainly from the decrease in the diffusion coefficient of  $\text{I}_3^-$ . This fact indicates that the interface between the PSE film and the Pt counter electrode is established in good condition because  $R_1$  would increase in the PSE-based DSSC otherwise.

### 3.2. The cell-gap dependence of the $J_{sc}$

Fig. 6 shows the dependence of the  $J_{sc}$  on the cell gap of the liquid electrolyte-based and PSE-based DSSCs. The dependence of the  $J_{sc}$  becomes weaker in a narrower cell-gap region. The  $J_{sc}$  of liquid electrolyte (GBL)-based DSSC is almost constant in cell gaps less than 50  $\mu\text{m}$ , whereas that of the PSE (GBL/matrix polymer = 37.0 mass%)-based DSSC monotonically decreases with the cell gap in the cell-gap region studied. The difference in the cell-gap dependence between the two kinds of DSSCs originates mainly from the difference in the diffusion coefficient. The diffusion coefficient of the PSE is, as given in Table 1, smaller by a factor of about 3.7 than that of the liquid electrolyte.

The melting points of PSE films and the  $J_{sc}$  of DSSCs with five different polymer contents are plotted in Fig. 7(a) and (b), respectively. Although the  $J_{sc}$  of PSE-based DSSCs increases as the polymer content decreases, the trade-off for decreasing the PVDF-HFP-based polymer content is the diminishment of the PSE tensile strength at high temperatures because the melting point drops. We then employed a PSE film with a 35 mass% polymer content and a 20  $\mu\text{m}$  cell gap, and we confirmed that the  $J_{sc}$  of a PSE-based DSSC reached about 97% of that of a liquid electrolyte-based DSSC. The PSE film used in this DSSC was selected to have a melting point of 95  $^{\circ}\text{C}$ , which is high enough for outdoor applications.

## 4. Conclusion

Electrochemical studies were performed on the two different kinds of DSSCs to explain why the conversion efficiency is lower in PSE-based DSSCs than in liquid electrolyte-based DSSCs. The difference in the  $J_{sc}$  between the two different kinds of DSSCs was found out to depend chiefly on the diffusion coefficient of  $\text{I}_3^-$ . The  $J_{sc}$  of the PSE-based DSSC has a strong dependence on the cell gap, and a narrower cell gap gives a higher  $J_{sc}$ . The  $J_{sc}$  of the PSE-based DSSC with the 20  $\mu\text{m}$  cell gap reaches the value comparable to that of the liquid electrolyte-based DSSC. This fact indicates that the conversion efficiency of the PSE-based DSSC can be improved even higher and equal to that of the liquid electrolyte-based DSSC by optimizing the DSSC structure as well as ingredient of PSE films.

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